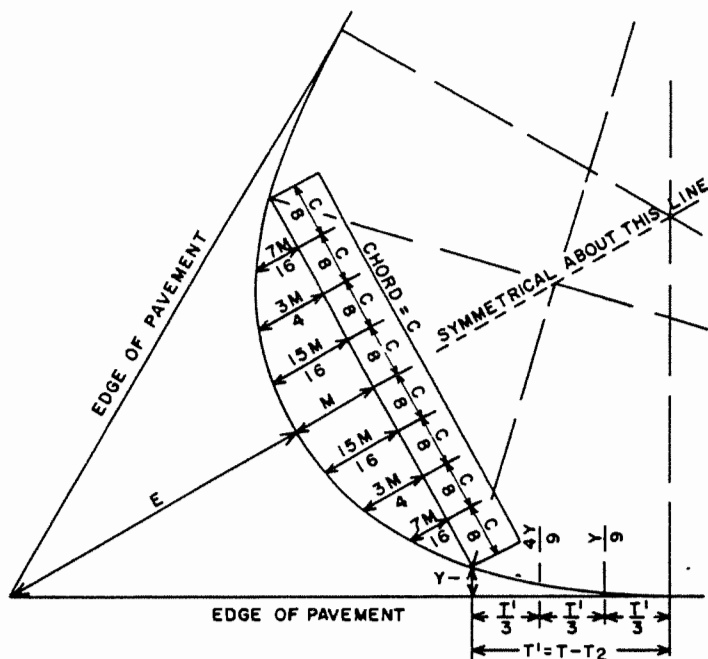




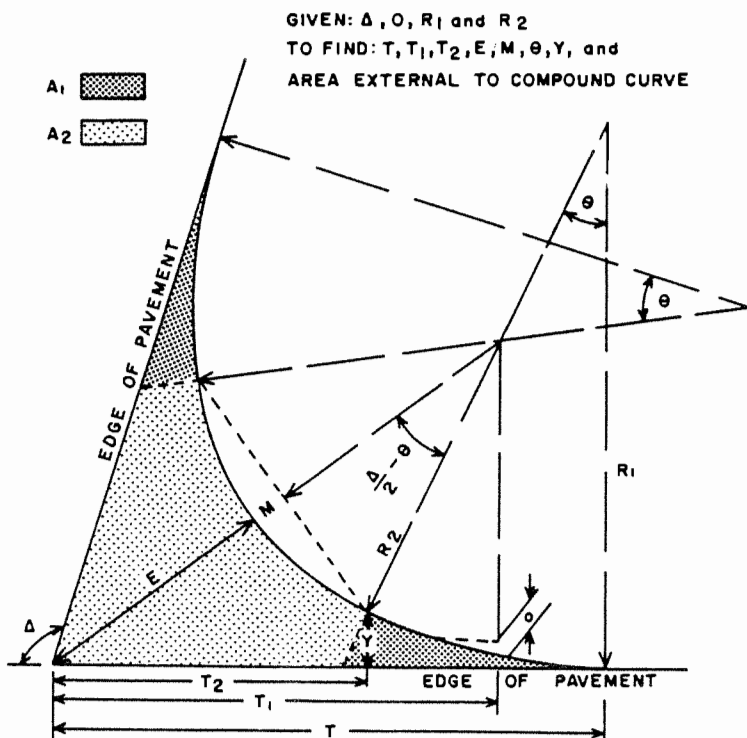
The following method is suggested for staking out 3-centred curves (when curve centres are inaccessible) by tangent offsets for the long radius curve and chord offsets for the short radius curve.

The curves are parabolic but any deviation from a circular curve is within tolerable limits.

The chord is determined by staking out the two points of compound curvature and then measuring the distance between these two points.

The Mid-Ordinate 'M' is determined by subtracting the External 'E' from the distance between the point of intersection of the two edges of pavement and the Mid-Point on the chord.

The value of 'M' may also be selected directly (or by interpolation) from Sheet 2.



GIVEN: Δ , O , R_1 and R_2
TO FIND: T_1 , T_2 , E , M , θ , Y , and
AREA EXTERNAL TO COMPOUND CURVE

FORMULAS USED

$$T_1 = (R_2 + O) \tan \frac{\Delta}{2}$$

$$T = T_1 + (R_1 - R_2) \sin \theta$$

$$T_2 = T_1 - R_2 \sin \theta$$

$$E = \frac{R_2 + O}{\cos \frac{\Delta}{2}} - R_2$$

$$M = R_2 - [R_2 \cos (\frac{\Delta}{2} - \theta)]$$

$$\theta = \cos^{-1} \frac{R_1 - R_2 - O}{R_1 - R_2}$$

$$Y = (R_2 + O) - R_2 \cos \theta$$

$$\text{AREA} = A_1 + A_2$$

$$A_1 = R_1^2 \tan \theta - \frac{\pi R_1^2 \theta}{180}$$

$$A_2 = (R_2 + O) \{ T_1 - (R_2 + O) \tan \theta \} - \frac{\pi R_2^2 (\frac{\Delta}{2} - \theta)}{180}$$

RECOMMENDED

APPROVED

DATE: SEPT. 7, 1976

ROAD DESIGN ENGINEER

CHIEF ENGINEER

SASKATCHEWAN DEPARTMENT OF HIGHWAYS

THREE-CENTRE CURVE FIELD LAYOUT METHOD

STANDARD
PLAN

No.

20605

SHEET 1 OF 2

CONSTANTS													CONSTANTS												
DEG.	T ₂	T ₁	T	E	M	AREA	CHORD	C/B	7M/16	3M/4	15M/16	DEG.	T ₂	T ₁	T	E	M	AREA	CHORD	C/R	7M/16	3M/4	15M/16		
LENGTH IN METRES													LENGTH IN METRES												
DESIGN VEH	55	5.52	12.55	19.57	4.17	0.33	48.30	7.76	0.97	0.14	0.25	0.31	DESIGN VEH.	75	7.06	9.67	15.11	3.88	1.12	28.68	10.11	1.26	0.49	0.84	1.05
WB-15	56	5.79	12.81	19.84	4.29	0.36	50.15	8.15	1.02	0.16	0.27	0.34	SU-9	76	7.23	9.84	15.29	3.99	1.16	29.64	10.30	1.29	0.51	0.87	1.09
R ₁ = 46	57	6.06	13.09	20.11	4.42	0.40	52.07	8.55	1.07	0.18	0.30	0.38	R ₁ = 37	77	7.41	10.02	15.47	4.10	1.21	30.63	10.49	1.31	0.53	0.91	1.13
R ₂ = 23	58	6.33	13.36	20.39	4.55	0.44	54.05	8.94	1.12	0.19	0.33	0.41	R ₂ = 12	78	7.59	10.20	15.65	4.21	1.25	31.66	10.68	1.33	0.55	0.94	1.18
O = 1.1	59	6.61	13.64	20.66	4.69	0.48	56.09	9.33	1.17	0.21	0.36	0.45	O = 0.6	79	7.77	10.39	15.83	4.33	1.30	32.71	10.87	1.36	0.57	0.98	1.22
θ = 17°47'30"	60	6.89	13.91	20.94	4.83	0.52	58.20	9.73	1.22	0.23	0.39	0.49	θ = 12°34'42"	80	7.96	10.57	16.02	4.45	1.35	33.80	11.05	1.38	0.59	1.01	1.26
T/3 = 4.69	61	7.17	14.20	21.22	4.97	0.56	60.37	10.12	1.26	0.25	0.42	0.53	T/3 = 2.69	81	8.15	10.76	16.21	4.57	1.40	34.92	11.24	1.40	0.61	1.05	1.31
Y = 2.20	62	7.45	14.48	21.51	5.12	0.61	62.62	10.51	1.31	0.27	0.46	0.57	Y = 0.89	82	8.34	10.95	16.40	4.70	1.45	36.06	11.42	1.43	0.63	1.08	1.36
Y/9 = 0.24	63	7.74	14.77	21.80	5.27	0.66	64.94	10.90	1.36	0.29	0.49	0.61	Y/9 = 0.10	83	8.53	11.15	16.59	4.82	1.50	37.27	11.61	1.45	0.65	1.12	1.40
4Y/9 = 0.98	64	8.03	15.06	22.09	5.42	0.70	67.33	11.29	1.41	0.31	0.53	0.66	4Y/9 = 0.39	84	8.73	11.35	16.79	4.95	1.55	38.50	11.79	1.47	0.68	1.16	1.45
	65	8.33	15.35	22.38	5.58	0.75	69.80	11.68	1.46	0.33	0.57	0.71		85	8.93	11.55	16.99	5.09	1.60	39.77	11.97	1.50	0.70	1.20	1.50
DESIGN VEH	65	6.37	12.55	22.16	5.36	0.42	67.04	7.75	0.97	0.18	0.32	0.40	DESIGN VEH.	85	8.93	11.55	16.99	5.09	1.60	39.77	11.97	1.50	0.70	1.20	1.50
WB-15	66	6.62	12.79	22.40	5.49	0.46	69.00	8.06	1.01	0.20	0.34	0.43	SU-9	86	9.14	11.75	17.19	5.23	1.65	41.09	12.15	1.52	0.72	1.24	1.55
R ₁ = 46	67	6.86	13.04	22.65	5.62	0.49	71.01	8.36	1.05	0.22	0.37	0.46	R ₁ = 37	87	9.34	11.96	17.40	5.37	1.71	42.44	12.33	1.54	0.75	1.28	1.60
R ₂ = 18	68	7.11	13.29	22.90	5.76	0.53	73.08	8.67	1.08	0.23	0.40	0.50	R ₂ = 12	88	9.55	12.17	17.61	5.52	1.76	43.84	12.51	1.56	0.77	1.32	1.65
O = 1.7	69	7.36	13.54	23.15	5.90	0.57	75.21	8.97	1.12	0.25	0.43	0.53	O = 0.89	89	9.77	12.38	17.83	5.67	1.81	45.28	12.69	1.59	0.79	1.36	1.70
θ = 20°04'05"	70	7.62	13.79	23.40	6.05	0.61	77.40	9.28	1.16	0.27	0.46	0.57	θ = 12°34'42"	90	9.99	12.60	18.04	5.82	1.87	46.77	12.87	1.61	0.82	1.40	1.75
T/3 = 5.26	71	7.88	14.05	23.66	6.20	0.65	79.65	9.58	1.20	0.28	0.49	0.61	T/3 = 2.69	91	10.21	12.82	18.27	5.98	1.93	48.31	13.04	1.63	0.84	1.45	1.81
Y = 2.79	72	8.14	14.31	23.92	6.35	0.69	81.97	9.88	1.24	0.30	0.52	0.65	Y = 0.89	92	10.43	13.05	18.49	6.14	1.98	49.90	13.22	1.65	0.87	1.49	1.86
Y/9 = 0.31	73	8.40	14.58	24.19	6.51	0.74	84.35	10.18	1.27	0.32	0.55	0.69	Y/9 = 0.10	93	10.66	13.28	18.72	6.30	2.04	51.54	13.39	1.67	0.89	1.53	1.91
4Y/9 = 1.24	74	8.67	14.85	24.45	6.67	0.78	86.80	10.48	1.31	0.34	0.59	0.73	4Y/9 = 0.39	94	10.90	13.51	18.96	6.48	2.10	53.24	13.57	1.70	0.92	1.58	1.97
	75	8.94	15.12	24.72	6.83	0.83	89.31	10.78	1.35	0.36	0.62	0.76		95	11.14	13.75	19.19	6.65	2.16	54.99	13.74	1.72	0.95	1.62	2.03
DESIGN VEH	75	9.15	14.96	24.00	6.58	0.95	82.72	11.52	1.44	0.41	0.71	0.89	DESIGN VEH.	95	10.31	12.66	18.21	6.17	2.01	47.80	12.67	1.58	0.88	1.51	1.88
WB-15	76	9.42	15.24	24.28	6.72	1.00	85.20	11.82	1.48	0.44	0.75	0.93	SU-9	96	10.53	12.88	18.44	6.34	2.06	49.34	12.83	1.60	0.90	1.55	1.93
R ₁ = 46	77	9.70	15.51	24.55	6.86	1.05	87.75	12.11	1.51	0.46	0.79	0.98	R ₁ = 37	97	10.76	13.11	18.66	6.51	2.12	50.93	12.98	1.62	0.93	1.59	1.99
R ₂ = 18	78	9.98	15.79	24.83	7.00	1.10	90.38	12.41	1.55	0.48	0.83	1.03	R ₂ = 12	98	10.99	13.34	18.90	6.68	2.18	52.58	13.14	1.64	0.95	1.63	2.04
O = 1.5	79	10.26	16.07	25.12	7.16	1.16	93.09	12.70	1.59	0.51	0.87	1.09	O = 0.6	99	11.23	13.58	19.14	6.86	2.23	54.28	13.29	1.66	0.98	1.66	2.09
θ = 18°50'21"	80	10.55	16.36	25.40	7.32	1.21	95.88	13.00	1.62	0.53	0.91	1.14	θ = 12°34'42"	100	11.47	13.82	19.38	7.05	2.29	56.03	13.44	1.68	1.00	1.72	2.15
T/3 = 4.95	81	10.84	16.65	25.70	7.48	1.27	98.74	13.29	1.66	0.56	0.95	1.19	T/3 = 2.69	101	11.72	14.07	19.63	7.24	2.35	57.85	13.60	1.70	1.03	1.76	2.20
Y = 2.46	82	11.14	16.95	25.99	7.64	1.33	101.70	13.58	1.70	0.58	1.00	1.25	Y = 0.89	102	11.98	14.32	19.88	7.43	2.41	59.73	13.75	1.72	1.05	1.81	2.26
Y/9 = 0.27	83	11.44	17.25	26.29	7.80	1.39	104.74	13.87	1.73	0.61	1.04	1.30	Y/9 = 0.10	103	12.23	14.58	20.14	7.63	2.47	61.67	13.89	1.74	1.08	1.85	2.32
4Y/9 = 1.10	84	11.75	17.56	26.60	7.96	1.45	107.88	14.16	1.77	0.63	1.09	1.36	4Y/9 = 0.39	104	12.50	14.85	20.40	7.84	2.53	63.68	14.04	1.76	1.11	1.90	2.37
	85	12.06	17.87	26.91	8.15	1.51	111.11	14.45	1.81	0.66	1.13	1.42		105	12.77	15.12	20.67	8.06	2.59	65.75	14.19	1.77	1.13	1.95	2.43
DESIGN VEH	85	10.51	15.12	24.65	7.38	1.36	87.31	12.49	1.56	0.60	1.02	1.28	DESIGN VEH.	105	10.66	13.16	20.93	7.59	1.75	62.51	10.68	1.33	0.77	1.32	1.65
WB-15	86	10.78	15.39	24.91	7.56	1.42	89.75	12.73	1.59	0.62	1.06	1.33	SU-9	106	10.91	13.40	21.17	7.78	1.80	64.24	10.80	1.35	0.79	1.35	1.69
R ₁ = 46	87	11.05	15.66	25.18	7.75	1.47	92.26	12.96	1.62	0.64	1.10	1.38	R ₁ = 37	107	11.15	13.65	21.42	7.98	1.85	66.02	10.93	1.37	0.81	1.39	1.73
R ₂ = 15	88	11.32	15.93	25.46	7.94	1.53	94.85	13.20	1.65	0.67	1.15	1.43	R ₂ = 12	108	11.40	13.90	21.67	8.18	1.90	67.86	11.05	1.38	0.83	1.42	1.78
O = 1.5	89	11.61	16.21	25.74	8.13	1.59	97.52	13.43	1.68	0.69	1.19	1.49	O = 0.6	109	11.66	14.16	21.93	8.39	1.95	69.76	11.18	1.40	0.85	1.46	1.82
θ = 17°53'48"	90	11.89	16.50	26.03	8.33	1.65	100.27	13.67	1.71	0.72	1.24	1.54	θ = 12°34'42"	110	11.93	14.42	22.20	8.61	1.99	71.72	11.30	1.41	0.87	1.50	1.87
T/3 = 4.71	91	12.18	16.79	26.32																					